

ME 4555 - Lecture 31 - Controller design using Bode ①

So far, we have used Bode plots to understand the frequency response of stable systems.

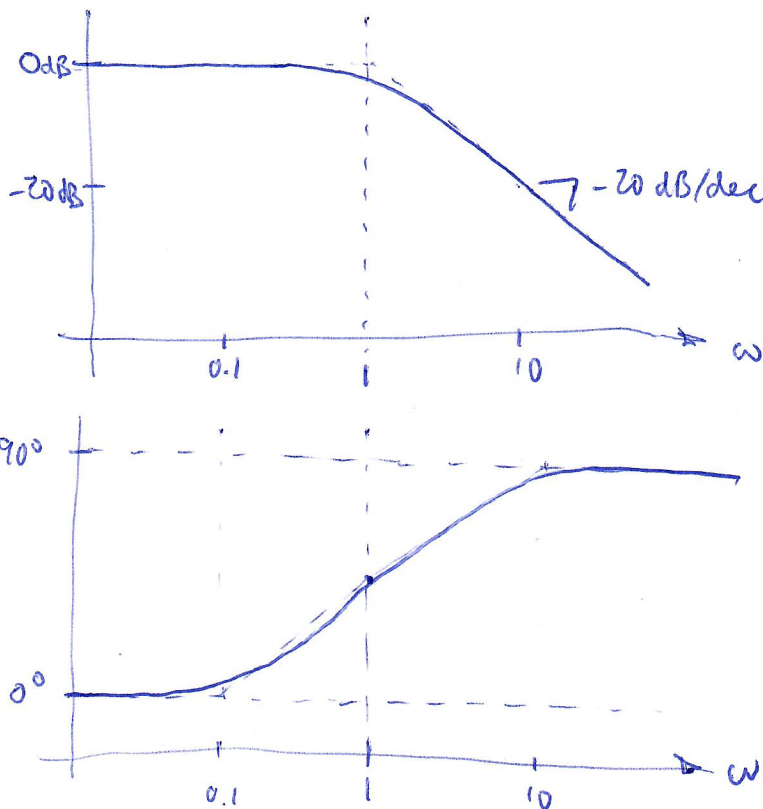
But what about unstable systems? We can still plot $M(\omega)$, $\phi(\omega)$ for an unstable system. For example: consider $G(s) = \frac{-1}{s-1}$

This is unstable (pole at $s=1$, in the right-half plane), yet we have

$$G(j\omega) = \frac{-1}{j\omega-1} = \frac{1}{1+\omega^2} + j \cdot \frac{\omega}{1+\omega^2} \Rightarrow \begin{cases} M(\omega) = \frac{1}{\sqrt{1+\omega^2}} \\ \phi(\omega) = \arctan \omega \end{cases}$$

so the Bode plot is:

Similar to a 1st order stable pole ($M(\omega)$ is the same as for $\frac{1}{s+1}$) but phase increases instead of decreasing!



However [important]

this Bode plot does not have the same interpretation as when the pole is stable!

Because: $e^{j\omega t} \xrightarrow{\frac{-1}{s-1}} \underbrace{M(\omega) e^{j(\omega t + \phi(\omega))}}_{\text{sinusoidal part}} - \underbrace{\frac{1+j\omega}{\omega^2+1} e^t}_{\text{transient}}$

this "transient" is unstable! so the output of our sinusoidal forcing is actually not a sinusoid in steady-state

Bode plots for unstable poles/zeros.

Note that a stable pole $\frac{1}{s+a}$ and an unstable pole $\frac{1}{s-a}$

Have the same magnitude:

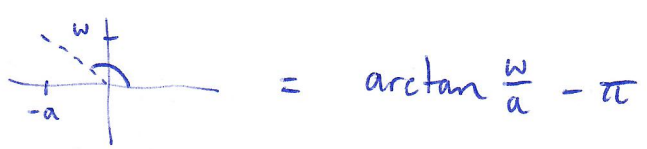
$$\left| \frac{1}{j\omega+a} \right| = \frac{1}{\sqrt{\omega^2+a^2}} \quad , \quad \left| \frac{1}{j\omega-a} \right| = \frac{1}{\sqrt{\omega^2+(-a)^2}} = \frac{1}{\sqrt{\omega^2+a^2}}$$

However, the phase is different:

$$\angle \left(\frac{1}{j\omega+a} \right) = -\angle(j\omega+a)$$



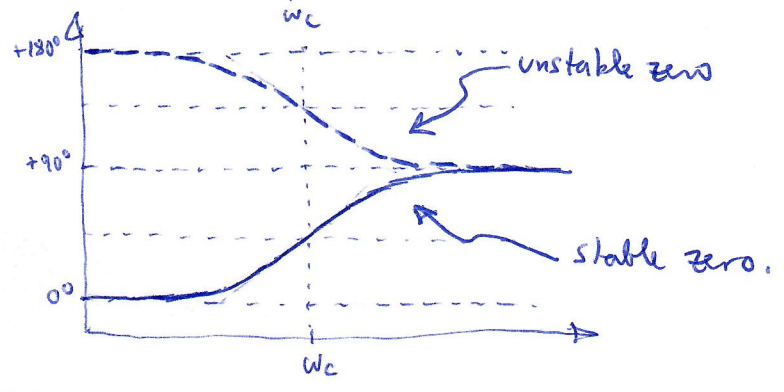
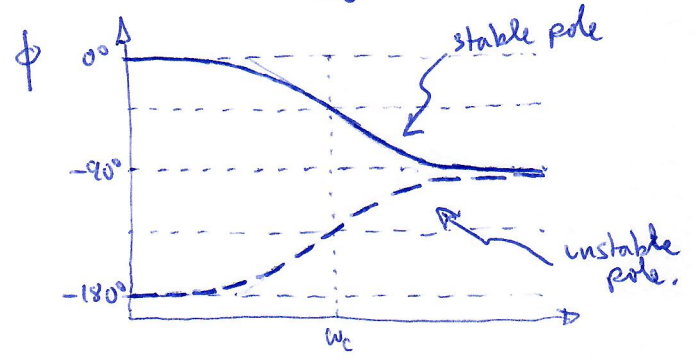
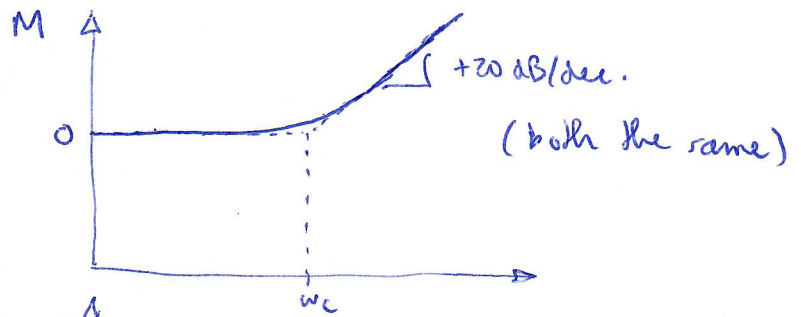
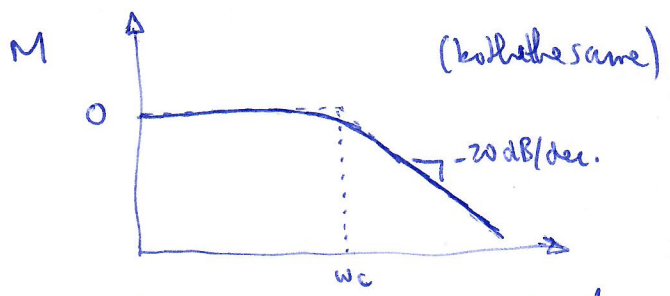
$$\angle \left(\frac{1}{j\omega-a} \right) = -\angle(j\omega-a)$$



Here is what the Bode plot looks like for an unstable/stable pole/zero.

real Pole: $\frac{1}{\frac{s}{\omega_c} \pm 1}$

real zero: $\left(\frac{s}{\omega_c} \pm 1 \right)$



NOTE: although it's possible to sketch the Bode plot for an unstable system, be careful about how you interpret it! The output to a sinusoidal input will be unbounded (transients do not dissipate)

Unstable zeros add more phase to a system than stable zeros do. This is why unstable zeros are often called "non-minimum phase zeros".

P-controllers using Bode

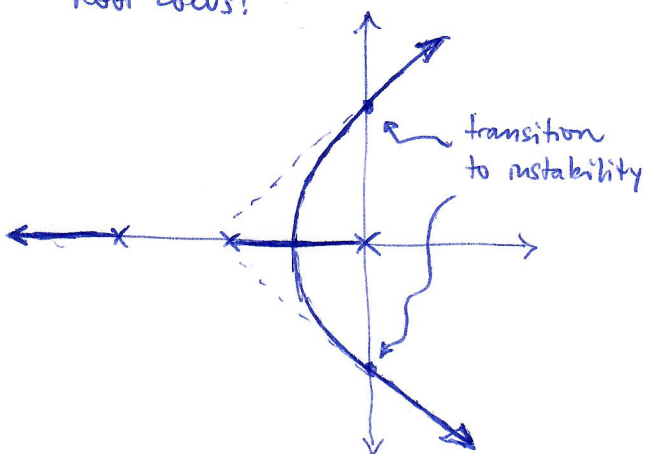
(2)

If our plant is $G(s)$ and we want to design a compensator $C(s) = K$ (P-controller), we want to know about the poles of the closed-loop system.

For now, assume $G(s)$ is stable. Then for small K , the closed loop is stable as well (think about root locus: \emptyset poles start at \emptyset poles. So if those are stable, then \emptyset poles are stable for small enough K). Transition to instability occurs when poles cross the $j\omega$ axis.

Ex: $G(s) = \frac{1}{s(s+1)(s+2)}$

Root locus:



At this critical transition to instability, there are poles that are purely imaginary.

i.e.: denominator of $\frac{GK}{1+GK}$ is zero

when $s = j\omega$ for some ω .

This means

$$K \cdot G(j\omega) = -1$$

But $G(j\omega)$ is the open loop Bode plot!

So instability occurs when $|K \cdot G(j\omega)| = 1$ and $\angle(K \cdot G(j\omega)) = -180^\circ$

Alternatively, we can write:

Instability occurs when $M(\omega) = \frac{1}{K}$ and $\phi(\omega) = -180^\circ$

So (a) find ω at which $\phi(\omega)$ crosses -180° . This is called the "phase crossover frequency". (b) Find $M(\omega)$ at this value of ω .

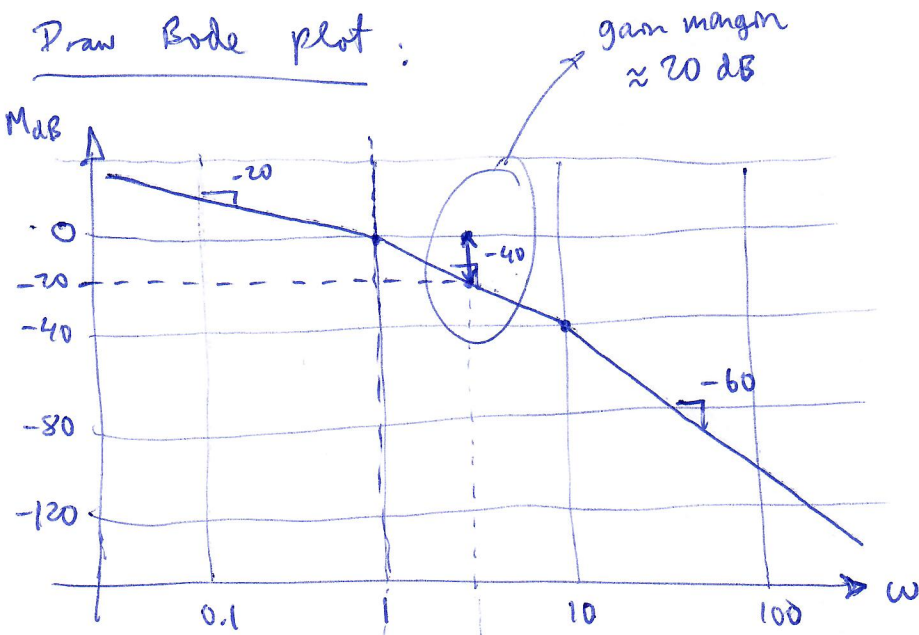
System is stable for $0 \leq K < \frac{1}{M(\omega)}$ — this is called the "gain margin".

Example: For what values of $C(s) = K$ is the closed-loop with

$$G(s) = \frac{1}{s(s+1)\left(\frac{s}{10}+1\right)} \text{ stable?}$$

(3)

Draw Bode plot:

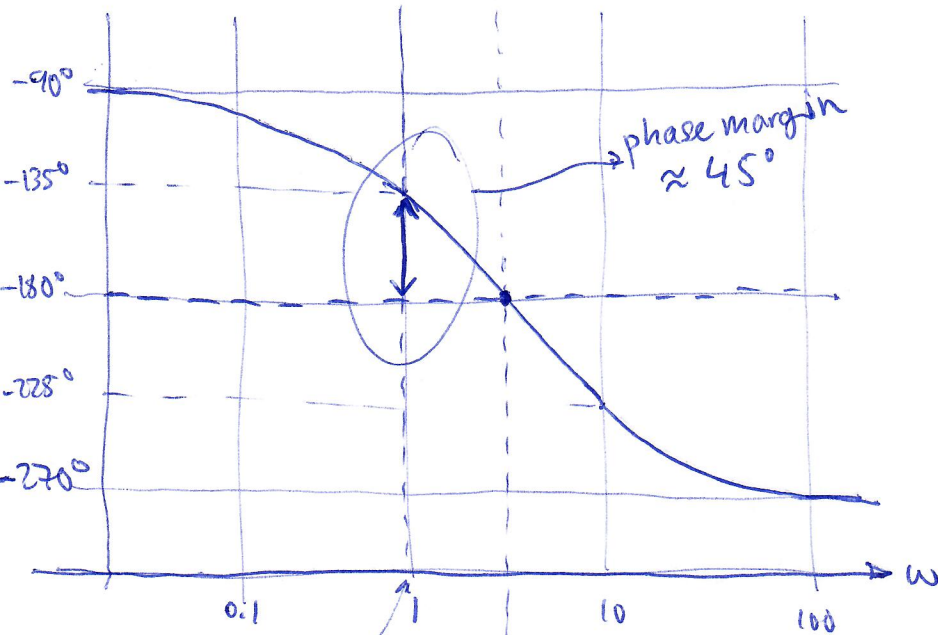


integrator \Rightarrow initial -20 dB/dec slope.

pole at $s = -1 \Rightarrow$ decrease to -40 dB/dec.

pole at $s = -10 \Rightarrow$ decrease to -60 dB/dec.

$\left\{ \begin{array}{l} -20 \text{ dB/dec per pole;} \\ \text{high-frequency rolloff} = -60 \text{ dB/dec.} \end{array} \right.$



integrator \Rightarrow initial phase is -90°

pole at $s = -1 \Rightarrow$ drop 90°

pole at $s = -10 \Rightarrow$ drop 90°

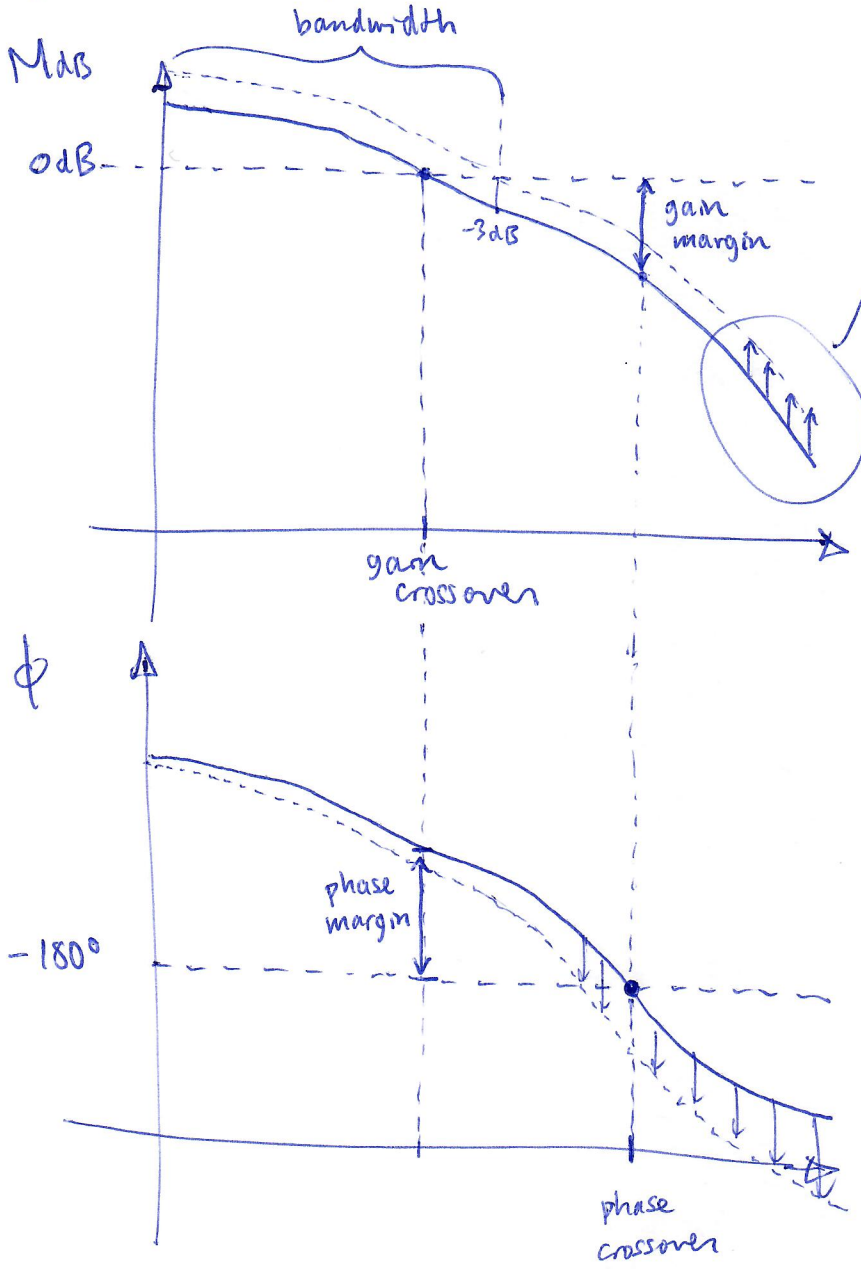
$\left\{ \begin{array}{l} -90^\circ \text{ per pole;} \\ \text{high frequency phase shift: } -270^\circ. \end{array} \right.$

gain crossover frequency ≈ 1 rad/sec.

phase crossover frequency ≈ 3.16 rad/sec.

Solution at -180° of phase, $M(\omega)$ is approximately -20 dB. So if we use a gain K , this shifts Magnitude plot upwards by $20 \log_{10} K$. We can tolerate a shift of up to 20 dB (i.e. $K = 10$). So system is stable in closed loop for $0 \leq K < 10$.

Gain and phase margins tell you about how much of a "safety buffer" you have between your system being stable vs unstable. Consider a typical low-pass filter:



Applying a constant gain K , shifts entire magnitude plot up

$$|K G(j\omega)| = |K| \cdot |G(j\omega)|$$

$$\Rightarrow \log_{10} |K G(j\omega)| = \underbrace{\log_{10} |K|}_{\text{translation}} + \log_{10} |G(j\omega)|$$

The gain margin (GM) is the largest gain we can use and still remain stable.

Note: $\mathcal{L}\{f(t-\tau)\} = e^{-s\tau} F(s)$
 delay of τ seconds.

So if there is a delay of τ seconds in the loop, we have $G(j\omega)$

becomes $e^{-j\omega\tau} G(j\omega)$

delay will cause a phase shift without affecting the magnitude.

phase due to delay is \downarrow

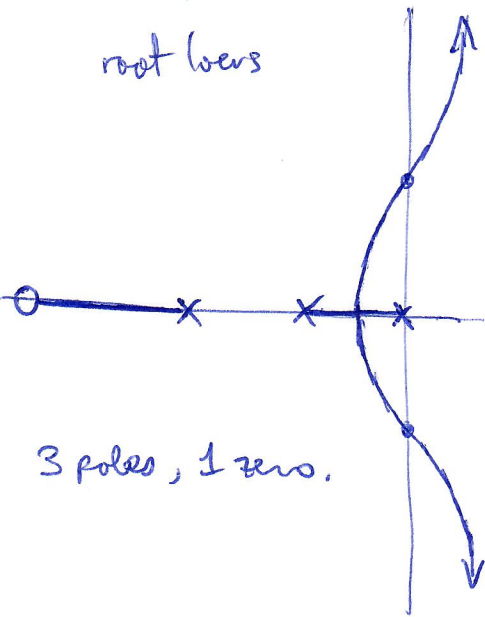
$$\angle \{e^{-j\omega\tau} G(j\omega)\} = \phi(\omega) - \tau\omega$$

★ having extra gain + phase margin allows you to be a bit wrong (margin of error) in your plant model and not risk going unstable. It makes your controller more robust.

★ there is a trade-off. Making K larger gives you more bandwidth (good thing) at the expense of stability.

Example

root locus



3 poles, 1 zero.

adding more gain

- increases the bandwidth
- causes the GM + PM to shrink
- causes the gain crossover and phase crossover frequencies to get closer together
- if K is increased too much, we have gain crossover $>$ phase crossover, which means instability.

even though there are 3 poles + 1 zero (vertical asymptotes) this might lead us to think that there is only $(3-1) \cdot (-90) = -180^\circ$ deg of phase and so we can't have instability. Not so! the three poles occur "first".

So the Bode plot looks like this:

